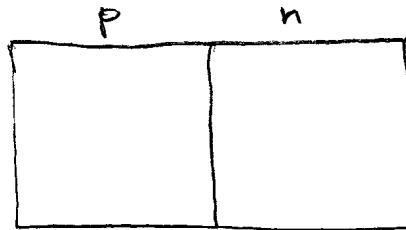


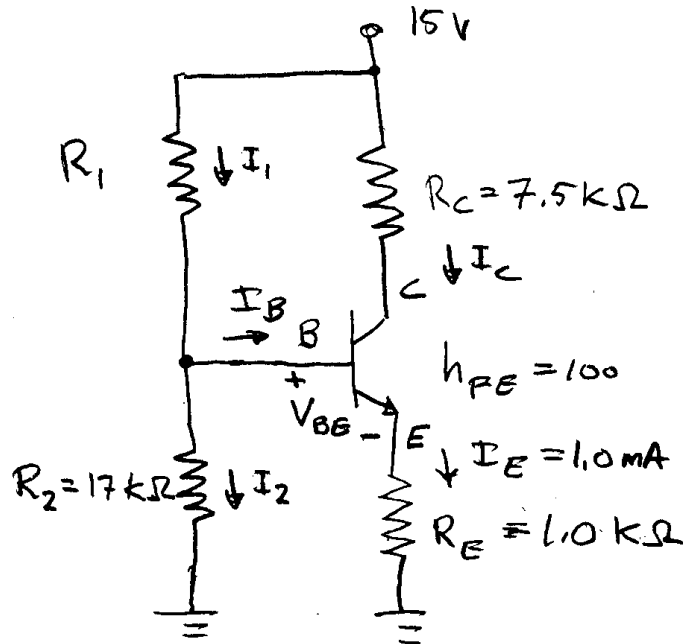
## Physics 116A Fall 2004: Exam 2

11/23/2004

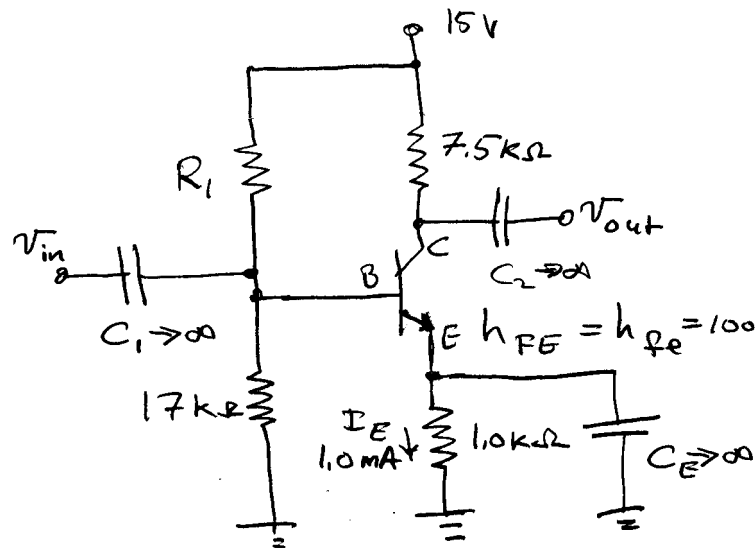
Closed book and notes except for two 8.5 in x 11 in sheets of paper. Show reasoning for full credit. There are 3 problems and 100 points.



1. ( $\approx 30$  points) The figure above shows an unbiased silicon  $pn$  junction at  $T = 300$  K. For Si at 300 K, the density of atoms is  $5 \times 10^{28} \text{ m}^{-3}$  and the intrinsic concentration is  $1.5 \times 10^{16} \text{ m}^{-3}$ . The free electron and hole mobilities are  $0.13 \text{ m}^2\text{V}^{-1}\text{s}^{-1}$  and  $0.05 \text{ m}^2\text{V}^{-1}\text{s}^{-1}$ , respectively. The magnitude of the electron charge,  $q$ , is  $1.6 \times 10^{-19} \text{ C}$ . At  $T = 300$  K,  $kT/q = 26 \text{ mV}$ .
  - (a) The n-type material is doped with one part per  $10^8$  of a donor impurity.
    - i. Find  $n_n$ , the electron concentration, **and**  $p_n$ , the hole concentration in the n-type bulk material (i.e., far from the junction).
    - ii. Find the conductivity,  $\sigma$ , of the n-type bulk material.
  - (b) Imagine that you could bring p-type and n-type materials together and join them to make the  $pn$  junction shown above. Consider the semiconductor region near the junction.
    - i. What physical process is responsible for an initial current of electrons from the n-type into the p-type material?
    - ii. After thermal equilibrium has been reached, there is no longer a net current across the junction. What has happened to oppose the initial current?
    - iii. Explain why a region depleted of mobile charge carriers is formed near the junction.
    - iv. Is the energy of the bottom edge of the conduction band the same in the p-type bulk material as it is in the n-type bulk material? Explain why or why not.



2. ( $\approx 30$  points) In the circuit above, assume  $R_1$  has the correct value for the BJT to be in the active region with  $I_E = 1.0$  mA (at least, as far as the base circuit is concerned).  $h_{FE} = 100$ .
- Find  $V_B$ . (Hint: first find  $V_E$  and use your estimate of  $V_{BE}$  in the active region.)
  - Find  $I_B$ .
  - Find  $I_1$ , the current in  $R_1$ .
  - Now find the value of  $R_1$ .
  - Find  $V_C$  and verify that the BJT is in the active region.



3. ( $\approx 40$  points) The Q point for this amplifier with  $I_E = 1.0$  mA was found in Problem 2. Capacitors have been added to make a common emitter amplifier. Use your calculated value for  $R_1$ . The emitter resistor has been bypassed with a large capacitor so that the BJT emitter voltage remains constant for small AC input signals. For the BJT,  $h_{fe} = 100$  and  $T = 300$  K.
- Draw the small signal AC equivalent circuit. Use the simple small-signal AC BJT model containing  $r_e$  and a current source. Assume all C's are infinite so they are short circuits for AC (not for DC, of course). **Use your small signal AC equivalent circuit to solve the following sub-problems.**
  - Evaluate  $r_e$  for this circuit.
  - Find an expression for  $v_{in}(= v_b)$  as a function of  $i_b$ . **Use this** to find  $R_b \equiv v_b/i_b$ , the effective resistance looking into the BJT base.
  - Find the input impedance of the circuit. Evaluate numerically.
  - Find an expression for  $v_{out}$  in terms of  $i_c$ .
  - Find the voltage gain,  $A_v \equiv v_{out}/v_{in}$ . Evaluate numerically.
  - One could have designed this amplifier to work with the same  $I_{EQ} = 1.0$  mA with  $R_E = 0$  by choosing different values of  $R_1$  and  $R_2$ . Then  $C_E$  would not have been needed. What is the advantage of using the circuit given above with nonzero  $R_E$ ? Hint: what would happen if the BJT temperature were to increase significantly?

1. (a) i.  $n_n = N_D = 5 \times 10^{28} \times 10^{-8} = \underline{5 \times 10^{20} \text{ m}^{-3}}$

$$p_n = \frac{n_i^2}{n_n} = \frac{(1.5 \times 10^{16})^2}{5 \times 10^{20}} \text{ m}^{-3} = 4.5 \times 10^{11} \text{ m}^{-3}$$

ii.  $\sigma = (n \mu_n + p \mu_p) q \approx n \mu_n q = 5 \times 10^{20} \text{ m}^{-3} \times 0.13 \text{ m}^2/\text{Vs} \times 1.6 \times 10^{-19} \text{ C}$   
 $= 10.4 \text{ } \Omega/\text{m}$

(b) i) diffusion

ii) Uncovered ions sets up  $\vec{E}$  field which sets up an opposing drift current.

iii) Electrons and holes occupying the region near the junction recombine, producing depletion region.

iv) No.  $\vec{E}$  field results in a "barrier" (or built-in) potential difference between the n and p material.

2.

(a)  $V_B = V_{BE} + V_E$   
 $= 0.7 \text{ V} + I_{E_Q} R_E$   
 $= 0.7 \text{ V} + 1 \text{ mA} \times 1 \text{ k}\Omega = \underline{1.7 \text{ V}}$

(b)  $I_B + I_C = I_E = 1.0 \text{ mA}$   
 $I_B + h_{FE} I_B = 1.0 \text{ mA}$   
 $I_B = 1.0 \text{ mA} / (h_{FE} + 1) = \frac{1.0 \text{ mA}}{101} = \underline{9.9 \text{ } \mu\text{A}}$

(c)  $I_1 = I_2 + I_B$ ,  $I_2 = V_B / 17 \text{ k}\Omega = \frac{1.7 \text{ V}}{17 \text{ k}\Omega} = \underline{100 \text{ } \mu\text{A}}$   
 $I_1 = 100 + 9.9 = \underline{110 \text{ } \mu\text{A}}$

(d)  $R_1 = (V_{CC} - V_B) / I_1 = (15 \text{ V} - 1.7 \text{ V}) / 110 \text{ } \mu\text{A} = \underline{121 \text{ k}\Omega}$

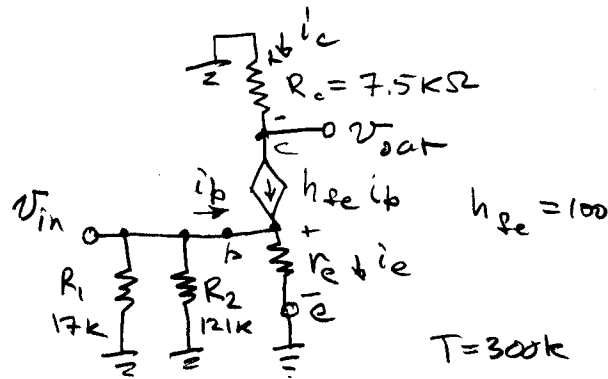
(e)  $V_C = V_{CC} - I_C R_C = 15 \text{ V} - h_{FE} I_B R_C = 15 \text{ V} - 100 \times 9.9 \text{ } \mu\text{A} \times 7.5 \text{ k}\Omega$   
 $= 15 \text{ V} - 7.4 \text{ V} = \underline{7.6 \text{ V}}$

For active region,  $V_{CE} > 0.2 \text{ V}$

$$V_{CE} = V_{C_Q} - I_{E_Q} R_E = 7.6 \text{ V} - 1 \text{ k}\Omega \times 1 \text{ mA}$$

$$= 7.6 - 1.0 = 6.6 \text{ V} > 0.2 \text{ V} \quad \underline{\text{OK}}$$

3. (a)



$$(b) r_e = \frac{kT}{q I_{E_Q}} = \frac{26 \text{ mV}}{I_{E_Q}} = \frac{26 \text{ mA} \cdot \Omega}{1.0 \text{ mA}} = \underline{26 \Omega}$$

$$(c) v_b = i_e r_e = (h_{fe} i_b + i_b) r_e = (h_{fe} + 1) i_b r_e$$

$$R_b \equiv \frac{v_b}{i_b} = (h_{fe} + 1) r_e = 101 \times 26 \Omega = \underline{2626 \Omega}$$

$$(d) R_{in} = R_b \parallel R_1 \parallel R_2 = \left[ \frac{1}{2626} + \frac{1}{17k} + \frac{1}{121k} \right]^{-1} \Omega$$

$$= \underline{2.2 \text{ k}\Omega}$$

$$(e) v_{out} = -i_c R_c$$

$$(f) A_v = \frac{v_{out}}{v_{in}} = \frac{-i_c R_c}{v_b} = \frac{-h_{fe} i_b R_c}{(h_{fe} + 1) i_b r_e}$$

$$= -\frac{h_{fe}}{h_{fe} + 1} \frac{R_c}{r_e} \approx -\frac{R_c}{r_e} = \frac{-7.5 \text{ k}\Omega}{26 \Omega} = \underline{-288}$$

(g)  $R_E$  provides bias stability.

If  $T$  increases,  $I_E$  increases for a given  $V_{BE}$ . But this increases the voltage drop across  $R_E$ , reducing  $V_{BE}$  (for fixed  $V_B$ ), decreasing  $I_E$  toward the desired  $I_{E_Q}$ .

Without  $R_E$ ,  $I_E$  could increase enough so the voltage drop across  $R_C (= \alpha I_E R_C)$  could take the BJT into saturation ( $V_{CE} \approx 0.2 \text{ V}$ ).