

Solution to Physics 108 MT (2015)

1-(1) From $S_o^{(1)} = +40 \text{ cm}$, $R_1 = +\infty$, $u_1 = 1$, $u_2 = 2$,
and

$$\frac{u_1}{S_o^{(1)}} + \frac{u_2}{S_i^{(1)}} = \frac{u_2 - u_1}{R_1}$$

$\Rightarrow S_i^{(1)} = -u_2 \cdot S_o^{(1)} = -80 \text{ cm}$. The image is formed at 80 cm to the left of the flat surface. Thus, $S_o^{(2)} = d - S_i^{(1)} = +100 \text{ cm}$, $R_2 = +50 \text{ cm}$, $u_1' = u_2 = 2$, $u_2' = u_2 = 2$, then

$$\frac{u_1'}{S_o^{(2)}} + \frac{u_2'}{S_i^{(2)}} = \frac{u_2' - u_1'}{R_2}$$

$$\text{or } \frac{2}{100 \text{ cm}} + \frac{1}{S_i^{(2)}} = \frac{1 - 2}{50 \text{ cm}}$$

$\therefore S_i^{(2)} = -25 \text{ cm}$, 25 cm to the left of the second surface

$$\begin{aligned} M &= M \left| \begin{array}{c} 1^{\text{st}} \text{ surface} \\ \text{---} \\ 2^{\text{nd}} \text{ surface} \end{array} \right| \\ &= \left(-\frac{u_1}{u_2} \frac{S_i^{(1)}}{S_o^{(1)}} \right) \cdot \left(-\frac{u_1'}{u_2'} \frac{S_i^{(2)}}{S_o^{(2)}} \right) = \frac{(-80)}{40} \cdot \frac{(-25)}{100} \\ &= +\frac{1}{2} \end{aligned}$$

1-(2)

$$\begin{aligned} \begin{pmatrix} A & B \\ C & D \end{pmatrix} &= \begin{pmatrix} 1 & 0 \\ \frac{2-1}{50} & 2 \end{pmatrix} \begin{pmatrix} 1 & 20 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & \frac{1}{2} \end{pmatrix} \\ &= \begin{pmatrix} 1 & 0 \\ \frac{1}{50} & 2 \end{pmatrix} \begin{pmatrix} 1 & 10 \\ 0 & \frac{1}{2} \end{pmatrix} \\ &= \begin{pmatrix} 1 & 10 \\ \frac{1}{50} & \frac{6}{5} \end{pmatrix} \end{aligned}$$

1-(3)

$$\begin{aligned} \sum_i^{(2)} &= - \frac{AS_0^{(1)} + B}{CS_0^{(1)} + D} \\ &= - \frac{40 + 10}{\frac{40}{50} + \frac{60}{50}} \\ &= -25 \text{ cm} \end{aligned}$$

(-4)

$$\begin{pmatrix} A & B \\ C & D \end{pmatrix}_{d \rightarrow 0} = \begin{pmatrix} 1 & 0 \\ \frac{1}{50} & 2 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ 0 & \frac{1}{2} \end{pmatrix}$$

$$= \begin{pmatrix} 1 & 0 \\ \frac{1}{50} & 1 \end{pmatrix}$$

$$= \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{pmatrix}$$

$$\therefore f = -50 \text{ cm.}$$

$$\begin{aligned} O_v \quad f &= \left(\frac{n_g - n_{air}}{n_{air}} \left(\frac{1}{R_1} - \frac{1}{R_2} \right) \right)^{-1} \\ &= \left(\frac{2-1}{1} \left(\frac{1}{\infty} - \frac{1}{50} \right) \right)^{-1} \\ &= \left(-\frac{1}{50} \right)^{-1} \end{aligned}$$

$$= -50 \text{ cm} \quad *$$

2-(1) Find the image of the van first.
 $s_o = 40 \text{ m}$, $R = +\infty$, from

$$\frac{1}{s_o} + \frac{1}{s_i} = -\frac{2}{R}$$

$s_i = -s_o = -40 \text{ m}$, i.e., 40 m behind the flat mirror.

$$y_i = y_o M = (2 \text{ m}) \cdot \left(-\frac{s_i}{s_o}\right) = +2 \text{ m}$$

The angular size to the image at 1 m in front of the mirror is

$$\alpha = \frac{y_i}{1 \text{ m} + 40 \text{ m}} = \frac{2}{41} = 0.049 \text{ radians}$$

2-(2) Now with $R = +80 \text{ m}$ and

$$\frac{1}{s_o} + \frac{1}{s_i} = -\frac{2}{R}$$

$\Rightarrow s_i = -20 \text{ m}$, i.e., 20 m behind the curved mirror.

$$y_i = y_o \cdot M = (2 \text{ m}) \cdot \left(-\frac{s_i}{s_o}\right) = +1 \text{ m}$$

$$\alpha' = \frac{y_i}{1 \text{ m} + 20 \text{ m}} = \frac{1}{21} = 0.048 \text{ radians}$$

2-(3) In this case, the van appears slightly farther away from the viewer than it actually is.

This effect is much more pronounced if R is much smaller than 80m . This is why the right side mirror on a car or any motor vehicle has a warning sign painted on the front surface.

3-a)

From

$$I_{\text{total}} = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos(\phi_1 - \phi_2)$$

and

$$I_{\text{max}} = I_1 + I_2 + 2\sqrt{I_1 I_2}$$

$$I_{\text{min}} = I_1 + I_2 - 2\sqrt{I_1 I_2}$$

Since the slit dimensions are the same, and the illumination is the same, I_1 and I_2 remain unchanged. So do I_{max} and I_{min} .

As to the fringe spacing ~~near~~ near the center of the screen,

$$\delta y = \left(\frac{x}{d}\right) \left(\frac{\lambda_0}{u}\right)$$

when d is reduced by a factor of 10, i.e., $d' = 10/d$,

$$\delta y' = \left(\frac{x}{d'}\right) \left(\frac{\lambda_0}{u}\right) = 10 \cdot \delta y$$

is increased by a factor of 10.

3-(2)

The thickness change in the air gap between two neighboring fringes is

$$sd = \frac{\lambda_0}{2 \cdot \cos \theta}$$

θ is the incident angle inside the gap, and should be the same as the viewing angle of 60° . Thus

$$sd = \frac{\lambda_0}{2 \cdot \cos 60^\circ} = \lambda_0.$$

~~Across~~ Across 10 fringes, we have 9 sd in the air gap thickness change

$$\Delta d \equiv 9sd = 9 \times (0.5 \mu\text{m}) = 4.5 \mu\text{m} \quad \#$$

3-(3)

At normal incidence, those wavelengths that yield minimum reflection satisfy

$$\frac{4\pi n}{\lambda_0} d = 2\pi \cdot m$$

$$\lambda_0 = \frac{1}{m} \cdot \frac{4}{3} (\mu\text{m})$$

Between $0.35 \mu\text{m}$ and $0.75 \mu\text{m}$, we have $\lambda_0 = \frac{2}{3} \mu\text{m}, \frac{4}{9} \mu\text{m} \quad \#$