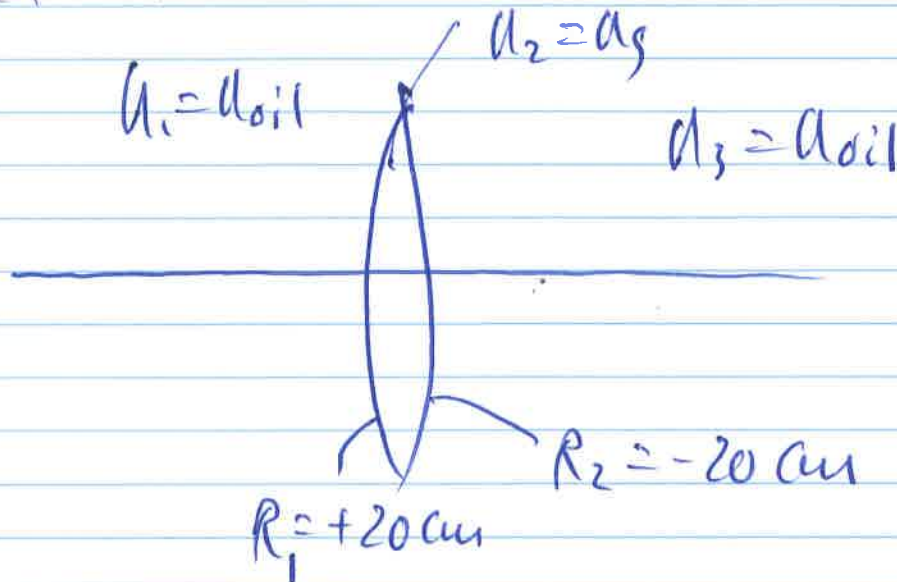


# Solutions to Physics 108 Final Exam. (Spring, 2021)

1. Thin lens:



Using the general thin lens equation,

$$\frac{n_1}{s_o} + \frac{n_3}{s_i} = \frac{n_2 - n_1}{R_1} + \frac{n_3 - n_2}{R_2} \quad \dots (1)$$

Since  $n_3 = n_1 = n_{oil}$ , this is reduced to

$$\frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{f} \quad \dots (2)$$

$$f = \frac{n_{oil}}{(n_g - n_{oil}) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)} = -40 \text{ cm}$$

It is a negative lens. From Eq. (2),

$$s_i = \frac{s_o \cdot f}{s_o - f} = (-) \cdot \frac{20 \text{ cm} \times 40 \text{ cm}}{20 \text{ cm} - (-40 \text{ cm})} = -\frac{40}{3} \text{ cm.}$$

The linear size of the virtual image  $g_i$  is

$$g_i = g_o \cdot m = g_o \left( -\frac{s_i}{s_o} \right)$$

(since  $d_3 = d_1$ )

$$= 2 \text{ mm} \times (-) \frac{(-40 \text{ cm}/3)}{20 \text{ cm}}$$

$$= + \frac{4}{3} \text{ mm.}$$

Or

$$g_i = g_o \cdot m = g_o \left( -\frac{f}{s_o - f} \right)$$
$$= 2 \text{ mm} \cdot (-) \cdot \frac{-40 \text{ cm}}{+60 \text{ cm}}$$

$$= + \frac{4}{3} \text{ cm}$$

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## 2. Diffraction:

2-1. The far-field diverging angle is

$$\Delta\theta = 2 \times \left( \lambda_0 / d \right) = \frac{2\lambda_0}{d}$$

At a distance  $L$  away, the beam diameter is given by

$$D = \Delta\theta \cdot L$$

with  $\lambda_0 = 0.5 \mu\text{m} = 5 \times 10^{-7} \text{m}$ ,  $d = 5 \text{cm} = 5 \times 10^{-2} \text{m}$ ,  
 $L = 1.61 \times 10^5 \text{m}$ ,

$$D = \frac{2 \times 5 \times 10^{-7} \text{m} \times 1.61 \times 10^5 \text{m}}{5 \times 10^{-2} \text{m}}$$

$$= 3.22 \text{m},$$

much larger than the original flashlight beam diameter. ~~##~~

2-2. We consider Fraunhofer diffraction along each direction separately.

Along x-direction,  $d_x = 100 \mu\text{m}$ . At  $L = 1 \text{ m}$  away, the width of the central bright feature along x direction on the screen is

$$D_x = 2 * L * \left( \frac{\lambda_0}{d_x} \right) = \frac{2 * 1 \text{ m} * 0.5 \mu\text{m}}{100 \mu\text{m}}$$
$$= 1 \text{ cm.}$$

Along y-direction,  $d_y = 20 \mu\text{m}$ . At  $L = 1 \text{ m}$ , the width of the central bright feature along y direction on the screen is

$$D_y = 2 * L * \left( \frac{\lambda_0}{d_y} \right) = \frac{2 * 1 \text{ m} * 0.5 \mu\text{m}}{20 \mu\text{m}}$$
$$= 5 \text{ cm}$$

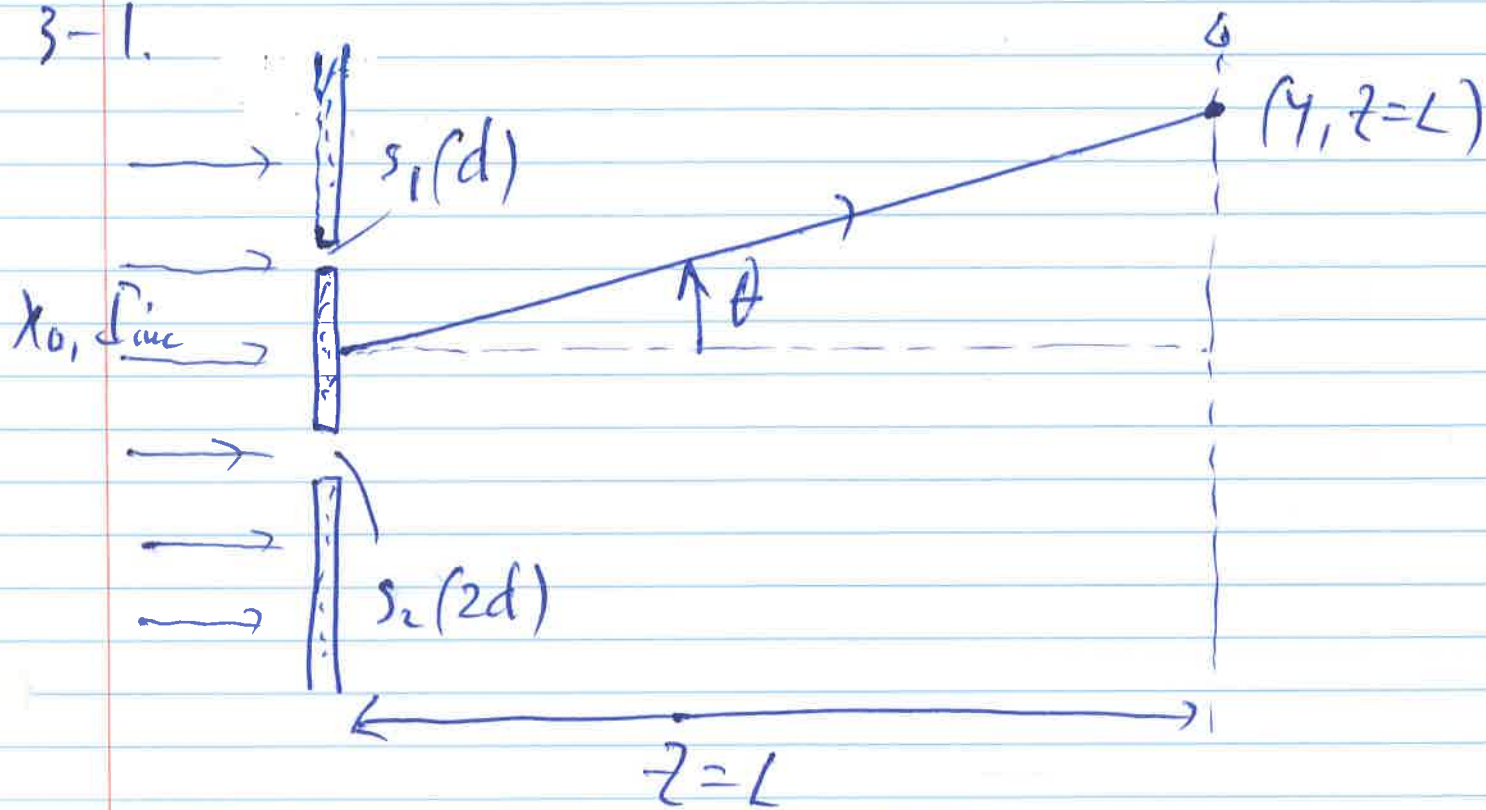
Thus,

$$\frac{D_x}{D_y} = \frac{d_y}{d_x}$$

i.e., the aspect ratio is reversed.

### 3. Single-slit diffraction and two-beam interference:

3-1.



$$I_1(\theta) = I_{inc} \left( \frac{d^2}{\lambda_0 L} \right) \cdot \frac{\sin^2 \left( \frac{\pi d}{\lambda_0} \sin \theta \right)}{\left( \frac{\pi d}{\lambda_0} \sin \theta \right)^2} \Bigg|_{d_1=d}$$

3-2.

$$I_2(\theta) = I_{inc} \left( \frac{(2d)^2}{\lambda_0 L} \right) \cdot \frac{\sin^2 \left( \frac{\pi \cdot 2d}{\lambda_0} \sin \theta \right)}{\left( \frac{\pi \cdot 2d}{\lambda_0} \sin \theta \right)^2} \Bigg|_{d_2=2d}$$

3-3.

$$I(\theta) = I_1(\theta) + I_2(\theta) + 2 \sqrt{I_1(\theta) I_2(\theta)} \cdot \cos\left(\frac{2\pi a}{\lambda_0} \sin\theta\right)$$

3-4.

$$I_2(\theta) = I_{inc} \left( \frac{4d^2}{\lambda_0 L} \right) \cdot \frac{\left( 4 \sin^2 \left( \frac{\pi d}{\lambda_0} \sin\theta \right) \cos^2 \left( \frac{\pi d}{\lambda_0} \sin\theta \right) \right)}{4 \left( \frac{\pi d}{\lambda_0} \sin\theta \right)^2}$$

$$= 4 \cos^2 \left( \frac{\pi d}{\lambda_0} \sin\theta \right) \cdot I_1(\theta)$$

Thus

$$I(\theta) = I_1(\theta) \left[ 1 + 4 \cos^2 \left( \frac{\pi d}{\lambda_0} \sin\theta \right) + 4 \left( \cos \left( \frac{\pi d}{\lambda_0} \sin\theta \right) \right) \times \cos \left( \frac{2\pi a}{\lambda_0} \sin\theta \right) \right]$$

When  $\theta \approx 0$ ,

$$I(\theta) = I_1(\theta) \cdot \left[ 5 + 4 \cos \left( \frac{2\pi a}{\lambda_0} \sin\theta \right) \right]$$

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#### 4. Reflection and transmission coefficients

4-1.  $n_1 = n_{\text{air}} = 1$ ,  $n_2 = n_{\text{water}} = 1.33$ ,  $\theta_1 = 60^\circ$ . From Snell's refraction law,  $n_1 \sin \theta_1 = n_2 \sin \theta_2$ ,

$$\theta_2 = \sin^{-1}(n_1 \sin \theta_1 / n_2) = 40.6^\circ$$

$$\cos \theta_1 = 0.50; \quad \cos \theta_2 = 0.76$$

$$R_s(\theta_1 = 60^\circ) = |r_s(\theta_1 = 60^\circ)|^2$$

$$= \left| \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2} \right|^2$$

$$= \left| \frac{0.5 - 1.33 \times 0.76}{0.5 + 1.33 \times 0.76} \right|^2 = 0.11$$

$$R_p(\theta_1 = 60^\circ) = |r_p(\theta_1 = 60^\circ)|^2$$

$$= \left| \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} \right|^2$$

$$= \left| \frac{0.76 - 1.33 \times 0.5}{0.76 + 1.33 \times 0.5} \right|^2 = 4.4 \times 10^{-3}$$

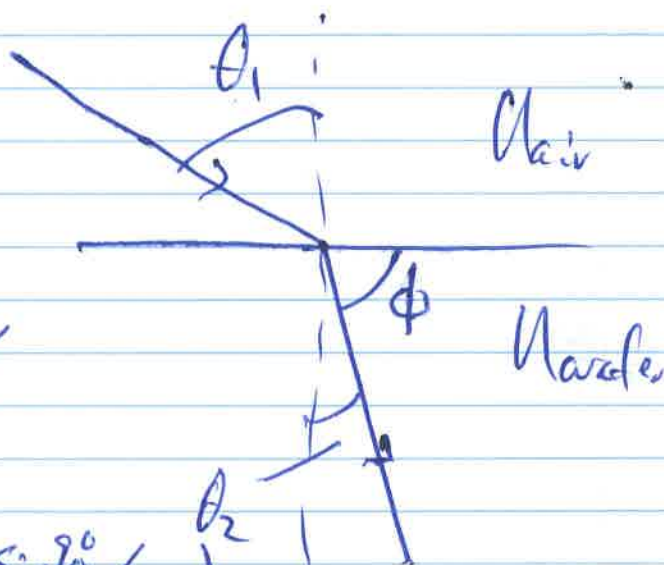
$$= 0.0044$$

4-2 The angle in the sea water from the plane of the water surface,  $\phi$ , is equal to  $90^\circ - \theta_2$  where  $\theta_2$  is the refraction angle of the light from an object above the water surface having an incidence angle  $\theta_1$ :

The largest  $\theta_2$  is obtained with  $\theta_1 \approx 90^\circ$ .

Thus the smallest  $\phi$  from the plane of the water surface is

$$\begin{aligned} \phi_{\min} &= 90^\circ - \theta_2(\text{Max}) \\ &= 90^\circ - \sin^{-1} \left( \frac{n_{\text{air}} \sin 90^\circ}{n_{\text{water}}} \right) \\ &= 90^\circ - \sin^{-1} \left( \frac{1}{n_{\text{water}}} \right) \\ &= 41.2^\circ \end{aligned}$$



So you need to lift the eye from the horizontal plane over  $41.2^\circ$  in order to start to see objects above the sea water.



4-3. For s-polarized light,

$$V_{s,12}(\theta_1=90^\circ) = \frac{n_1 \cos 90^\circ - n_2 \cos \theta_2}{n_1 \cos 90^\circ + n_2 \cos \theta_2}$$

$$= -1$$

$$\therefore R_s(\theta_1=90^\circ) = |V_{s,12}(\theta_1=90^\circ)|^2 = 1$$

For p-polarized light,

$$V_{p,12}(\theta_1=90^\circ) = \frac{n_1 \cos \theta_2 - n_2 \cos 90^\circ}{n_1 \cos \theta_2 + n_2 \cos 90^\circ}$$

$$= +1$$

$$\therefore R_p(\theta_1=90^\circ) = |V_{p,12}(\theta_1=90^\circ)|^2$$

$$= 1$$

Even when  $n_2$  is complex, or  $n_2$  is less than  $n_1$ , such that  $\cos \theta_2$  is complex,  $V_{s,12}(\theta_1=90^\circ) = -1$ , and  $V_{p,12}(\theta_1=90^\circ) = +1$ , thus

$$R_s(\theta_1=90^\circ) = R_p(\theta_1=90^\circ) = 1$$

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## 5. Polarization:

5-1. (a)

$$\begin{pmatrix} e^{i\pi/4} \\ e^{-i3\pi/4} \end{pmatrix} = e^{i\pi/4} \begin{pmatrix} 1 \\ e^{-i\pi} \end{pmatrix} = \sqrt{2} e^{i\pi/4} \begin{pmatrix} 1/\sqrt{2} \\ -1/\sqrt{2} \end{pmatrix}$$

It is a linearly polarized along an angle from the x-axis

$$\alpha = \tan^{-1} \left( \frac{-1/\sqrt{2}}{+1/\sqrt{2}} \right) = -45^\circ$$

$$(b) \begin{pmatrix} -1+i \\ -i-1 \end{pmatrix} = \begin{pmatrix} \sqrt{2} e^{i3\pi/4} \\ \sqrt{2} e^{i5\pi/4} \end{pmatrix} = 2 e^{i3\pi/4} \begin{pmatrix} 1/\sqrt{2} \\ i/\sqrt{2} \end{pmatrix}$$

It is a left-circularly polarized light.

$$(c) \begin{pmatrix} 4i \\ 2+2i \end{pmatrix} = \begin{pmatrix} 4 e^{i\pi/2} \\ 2\sqrt{2} e^{i\pi/4} \end{pmatrix} = \sqrt{24} e^{i\pi/2} \begin{pmatrix} \sqrt{2/3} \\ \sqrt{1/3} e^{-i\pi/4} \end{pmatrix}$$

It is an elliptically polarized light.

S-2.

$$\tilde{E}_{out} = \tilde{E}_L + e^{i\delta} \tilde{E}_R$$

$$= \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix} + e^{i\delta} \cdot \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -i \end{pmatrix}$$

$$= e^{i\delta/2} \frac{1}{\sqrt{2}} \begin{pmatrix} e^{i\delta/2} + e^{-i\delta/2} \\ (-i)(e^{i\delta/2} - e^{-i\delta/2}) \end{pmatrix}$$

$$= e^{i\delta/2} \cdot \sqrt{2} \cdot \begin{pmatrix} (e^{i\delta/2} + e^{-i\delta/2})/2 \\ (e^{i\delta/2} - e^{-i\delta/2})/2i \end{pmatrix}$$

$$= \left( \sqrt{2} e^{i\delta/2} \right) \begin{pmatrix} \cos \delta/2 \\ \sin \delta/2 \end{pmatrix}$$

It is a linearly polarized light, making an angle  $\alpha$  from the  $x$ -axis:

$$\alpha = \delta/2$$

## 6. Polarizing devices

$$6-1. \quad \vec{E} \approx \begin{pmatrix} \cos(-120^\circ) \\ \sin(-120^\circ) \end{pmatrix} = \begin{pmatrix} -1/2 \\ -\sqrt{3}/2 \end{pmatrix}$$

$$6-2. \quad \vec{E}_{inc} \approx \begin{pmatrix} \cos(-45^\circ) \\ \sin(-45^\circ) \end{pmatrix} = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -1 \end{pmatrix}$$

$$M_{QWP}(\text{FA} \parallel x\text{-axis}) = \begin{pmatrix} 1 & 0 \\ 0 & i \end{pmatrix}$$

$$\vec{E}_{out} \approx M_{QWP}(\text{FA} \parallel x\text{-axis}) \vec{E}_{inc}$$

$$= \begin{pmatrix} 1 & 0 \\ 0 & i \end{pmatrix} \begin{pmatrix} 1/\sqrt{2} \\ -1/\sqrt{2} \end{pmatrix}$$

$$= \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ i \end{pmatrix}$$

It is a right-circularly polarized light.

$$6-3. \quad \tilde{E}_{inc} = \begin{pmatrix} \cos 90^\circ \\ \sin 90^\circ \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

$$\begin{aligned} M_{HWP} (\text{PAO} + 45^\circ \text{ for } x\text{-axis}) \\ &= \begin{pmatrix} \cos(2 \times 45^\circ) & \sin(2 \times 45^\circ) \\ \sin(2 \times 45^\circ) & -\cos(2 \times 45^\circ) \end{pmatrix} \\ &= \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix} \end{aligned}$$

Thus

$$\begin{aligned} \tilde{E}_{out} &= M_{HWP} \tilde{E}_{inc} \\ &= \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \end{pmatrix} \end{aligned}$$

It is a linearly polarized light along x-axis